# *IVEM Investigation of Defect Evolution in FCC Compositionally Complex Alloys under Dual-Beam Heavy-Ion Irradiation*

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onventional nuclear structural alloys degrade severely after hundreds of displacements per atom, inadequately meeting the needs of next-generation fast reactors and triggering an investigation of compositionally complex alloys (CCA). Preliminary studies have shown that these alloys exhibit excellent mechanical properties and irradiation tolerance at hightemperature, promoting their candidacy for cladding and duct applications [1-20]. To investigate the fundamental mechanisms underlying the radiation resistance of compositionally complex base matrices, in situ dual-beam irradiations were performed on Cr<sub>18</sub>Fe<sub>27</sub>Mn<sub>27</sub>Ni<sub>28</sub> and Cr<sub>15</sub>Fe<sub>35</sub>Mn<sub>15</sub>Ni<sub>35</sub> at two elevated temperatures. Bubble populations were characterized at various dpa steps and compared to less compositionally complex reference materials.

## Experimental or Technical Approach

Electropolished discs of Cr<sub>18</sub>Fe<sub>27</sub>Mn<sub>27</sub>Ni<sub>28</sub> and Cr<sub>15</sub>Fe<sub>35</sub>Mn<sub>15</sub>Ni<sub>35</sub> were irradiated in situ using the 300 keV Hitachi-9000 TEM at the **IVEM-Tandem facility at Argonne** National Laboratory (ANL) using a 1 MeV Kr<sup>2+</sup> and 16 keV He<sup>+</sup> dual-ion beam with a He/dpa ratio of 0.75%/ dpa. Alloy selection, fabrication, preparation, precharacterization, and stopping range of ions in matter (SRIM) software inputs are detailed in references [11] and [3]. Pure Ni and a single-phase Fe<sub>56</sub>Ni<sub>44</sub> binary alloy were used for reference against the two FCC CCAs. Two irradiation temperatures were selected: 500°C and 600°C. All irradiations but one were performed up to 7 dpa, as estimated by IVEM-developed correlations between counts measured by a Faraday cup and both SRIM and Iradina calculations for the dpa through a 100 nm-thick specimen [21, 22]. The 500°C Ni irradiation was performed to 1 dpa with a He/dpa ratio of 1%/dpa, as detailed in reference [23]. Dpa profiles for combined and individual ion species and He implantation are



shown in Figure 1. Bubble formation was confirmed using underfocused and overfocused conditions. Bubble diameters were measured using ImageJ software and used to calculate swelling levels. Lamellae thicknesses were measured by direct electron method (K2 camera) and a slit width of 15 eV.

#### Results

The bubble population for all materials at both temperatures at their final dpa is shown in Figure 2. The average bubble diameters, bubble number densities, and swelling levels are plotted in Figure 3. For each material, bubbles nucleate with higher density and with a smaller size at 500°C relative to 600°C, and the average diameter of bubbles remains higher at 600°C up to the maximum dpa. Due to the high density of bubble nucleation at 500°C, the swelling

in Cr<sub>18</sub>Fe<sub>27</sub>Mn<sub>27</sub>Ni<sub>28</sub> is slightly higher than at 600°C despite the limited bubble size (<2 nm diameter), which contrasts with the pure Ni and Fe<sub>56</sub>Ni<sub>44</sub> binary alloy that exhibit significantly higher swelling at 600°C. The swelling levels in Cr<sub>15</sub>Fe<sub>35</sub>Mn<sub>15</sub>Ni<sub>35</sub> at both temperatures are comparable; this indicates that although mobility is increased at 600°C, similar quantities of vacancies and interstitials can arrive at both bubbles and other sinks. Between the two temperatures, the bubble densities in Cr<sub>15</sub>Fe<sub>35</sub>Mn<sub>15</sub>Ni<sub>35</sub> are closer together than were seen in Cr<sub>18</sub>Fe<sub>27</sub>Mn<sub>27</sub>Ni<sub>28</sub>, which demonstrates a reduced temperature effect on the mobility of vacancies and He atoms. Swelling levels in the two CCAs are consistently lower than the less compositionally complex materials. Figure 1.  $Kr^{2+}$  and  $He^+$  dpa and implantation profile for  $Cr_{18}Fe_{27}Mn_{27}Ni_{28}$  generated by SRIM. Average of 1 dpa within first 100 nm.  $Kr^{2+}$  ions are high enough in energy to pass through the samples with minimal implantation.



Figure 2. Bright-field micrographs of irradiated microstructures at final dpa of 1 dpa for pure Ni at 500°C [23] and 7 dpa for all other samples.

#### **Discussion/Conclusion**

Under favorable void-swelling conditions (i.e., dual-beam and hightemperature), bubbles nucleated in all irradiated materials. Under single-beam irradiation at 50 K, it was shown that Cr<sub>18</sub>Fe<sub>27</sub>Mn<sub>27</sub>Ni<sub>28</sub> and Cr<sub>15</sub>Fe<sub>35</sub>Mn<sub>15</sub>Ni<sub>35</sub> experienced a lower primary point defect production term than pure Ni and E90, a FeNiCr ternary alloy [11]. This reduction likely slowed bubble growth in CCAs compared to pure Ni and Fe<sub>56</sub>Ni<sub>44</sub>. Reference [23] proposed that vacancies generated in pure Ni under dual-beam conditions trap He atoms, leading to uniform nucleation of bubbles. In CCAs, the more localized and denser bubble nucleation is attributed to a distorted lattice, further trapping vacancies and He atoms.



Figure 3. (a) Average diameter, (b) number density, and (c) calculated swelling of irradiated materials with zoomed in swelling axis on the right for clarity.

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### **Publications**

[1.] Parkin, C., et al. (under review)., "Microstructural Evolution of Compositionally Complex Solid-Solution Alloys under Dual-Beam Irradiation.", Acta Materialia.

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NSUF Institution	Facilities and Capabilities
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