

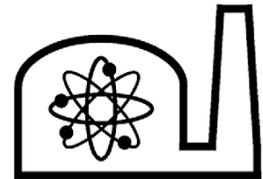
# *Advanced Cladding Irradiation Experiment at the MITR-II*

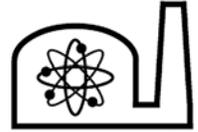
**David Carpenter**  
*Research Scientist*

ATR NSUF Users Week 2012



*MIT Nuclear Reactor Laboratory*





# Support and Collaborators

## □ *Support*

*ATR National Scientific User Facility*

*U.S. Department of Energy*

## □ *Collaborators*

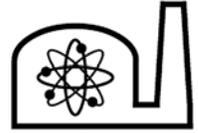
*Ceramic Tubular Products*

*Gamma Engineering Corporation*

*Westinghouse Electric Company*

*Oak Ridge National Laboratory*

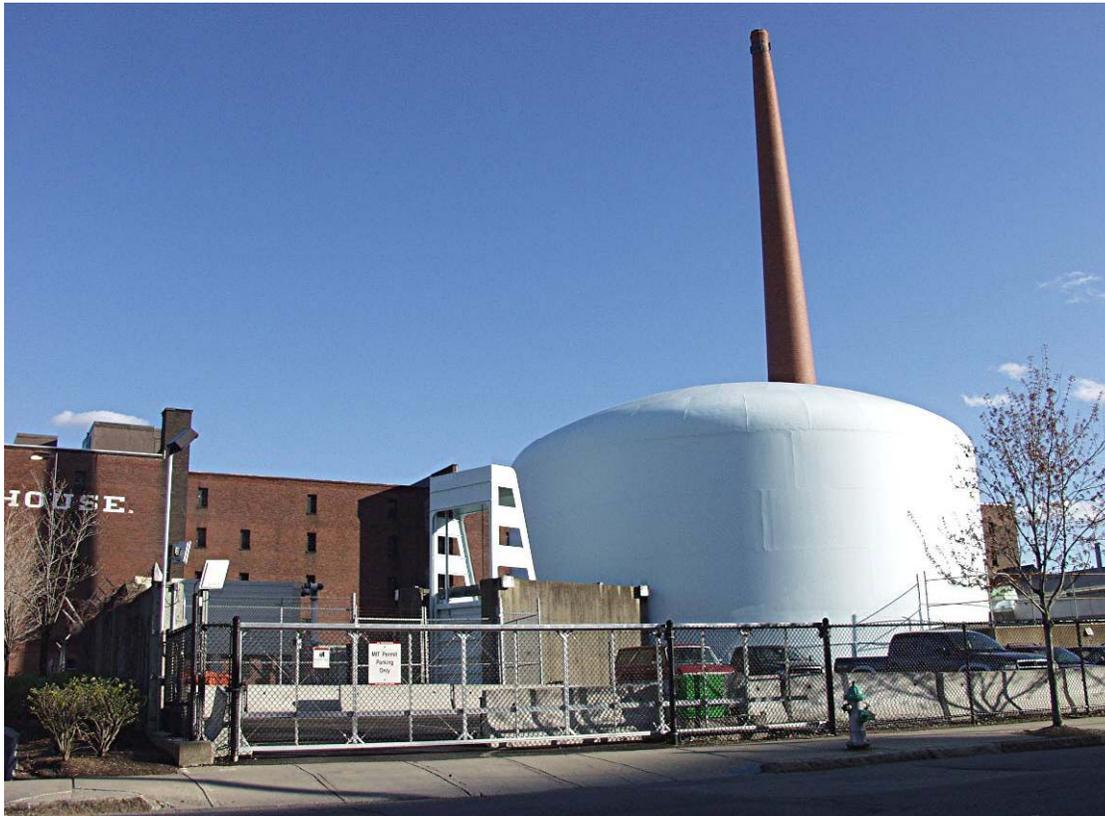
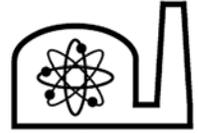
*Electric Power Research Institute*



# Outline

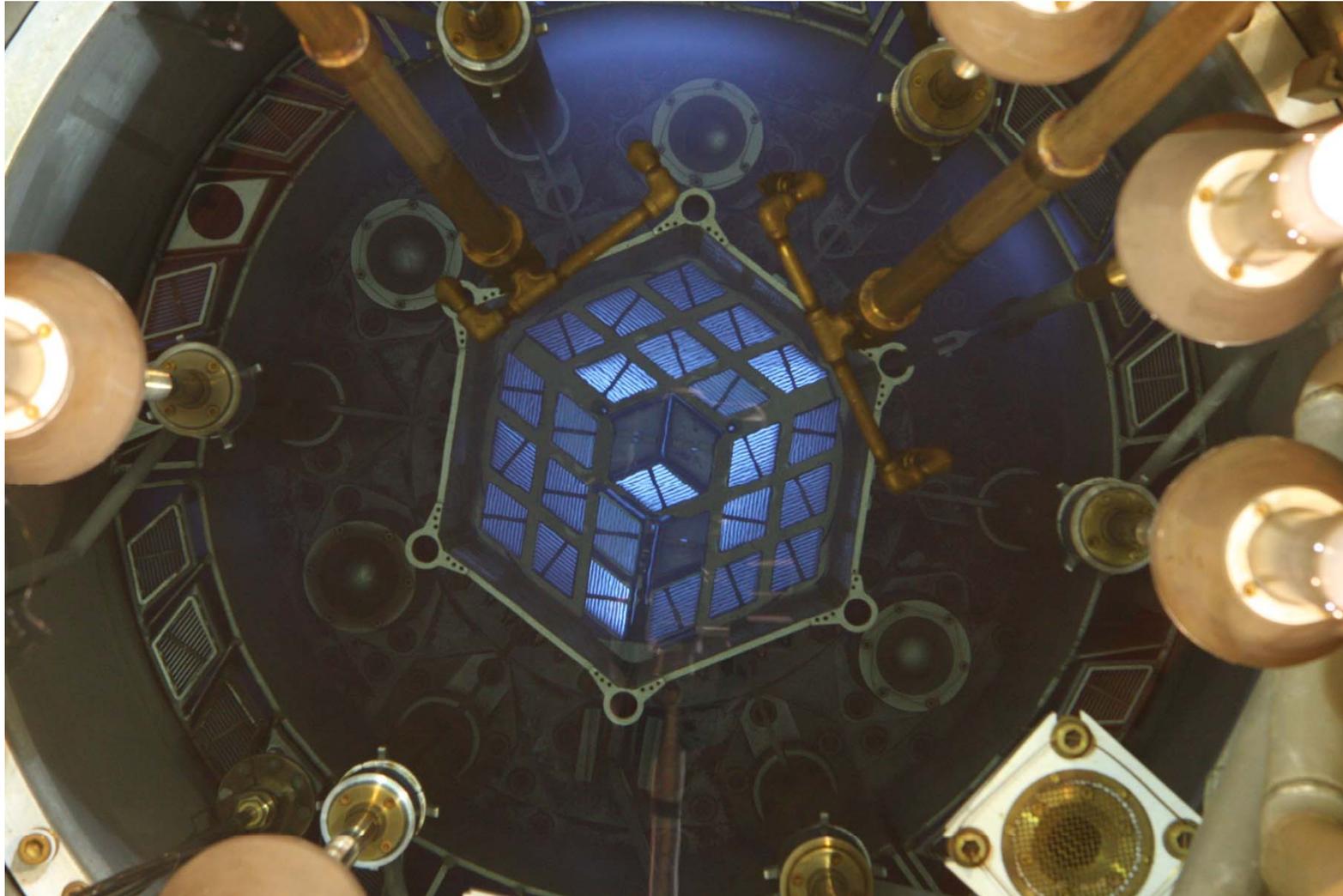
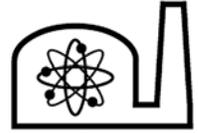
- ❑ Description of the MITR-II
- ❑ Intro to SiC for LWR cladding
- ❑ The ACI experiment

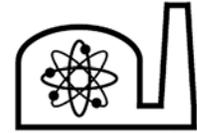
# MIT Nuclear Reactor Laboratory



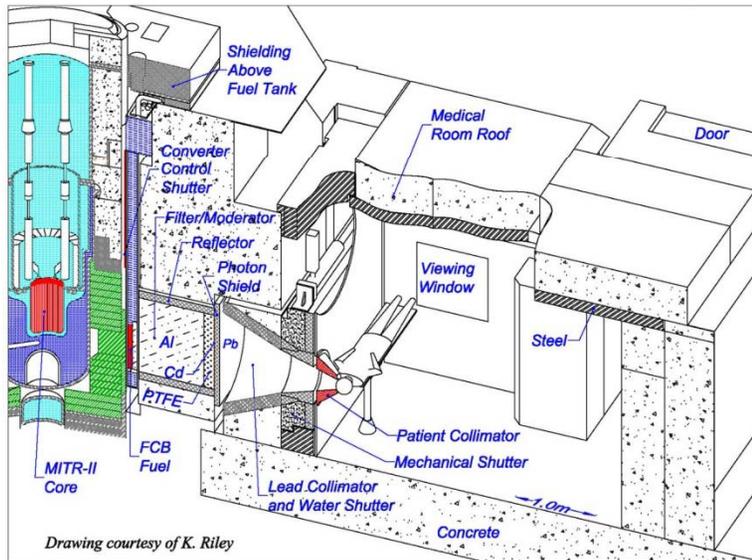
- ❑ MITR-II Reactor
  - Operating since 1958
  - Upgraded in 1975
- ❑ Operates 24/7 up to 6 MW thermal power
- ❑ Light water-cooled, heavy water-reflected
- ❑ HEU U-Al plate core
- ❑ Provides irradiation for research, education, and industry

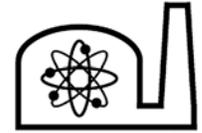
# Top-down View of the Core Tank



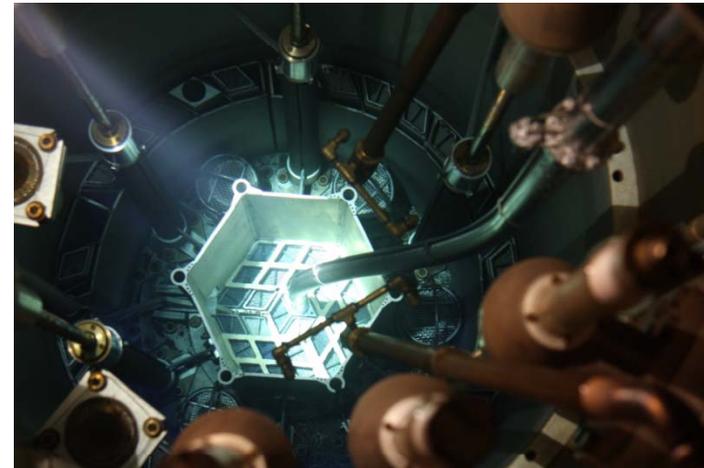
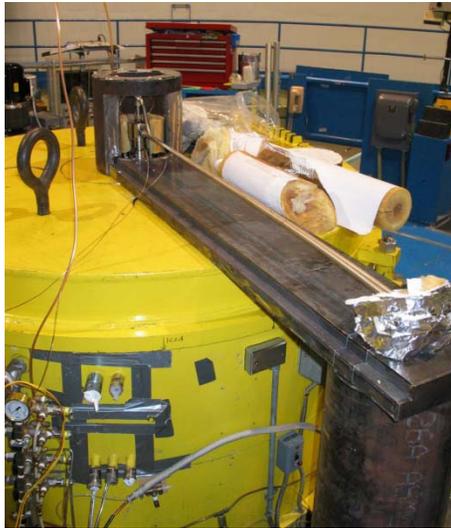


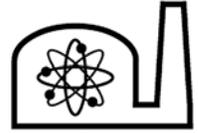
# Reactor Facilities





# In-Core Experiments



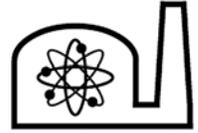


# Current and Planned ICEs

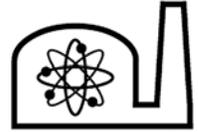
- ❑ ACI
  - SiC LWR cladding in PWR conditions
- ❑ HYFI
  - U-Zr-H LWR fuel rods with liquid metal bonding
- ❑ ICSA-Drexel
  - MAX-phase materials at 300-700°C in inert gas
- ❑ ICSA-LUNA
  - Fiber optics at 700°C in inert gas
- ❑ HTIF-LUNA
  - On-line reading fiber optics at 1200°C in inert gas
- ❑ ICSA-FHR
  - Ceramic and metal coupons in FLiBe salt at 700°C
- ❑ FHR Natural Circulation
  - Ceramic and metal coupons in flowing FLiBe salt at 700°C



# Motivation for New LWR Cladding



- ❑ Desire to improve fuel cladding performance in current and future light water reactors.
- ❑ Reactor operation is limited by the properties of current zirconium-based claddings and the resulting regulatory environment.
- ❑ Fukushima.
- ❑ Silicon carbide cladding may allow LWR fuel rods to be run to higher burnup and with better safety margins.

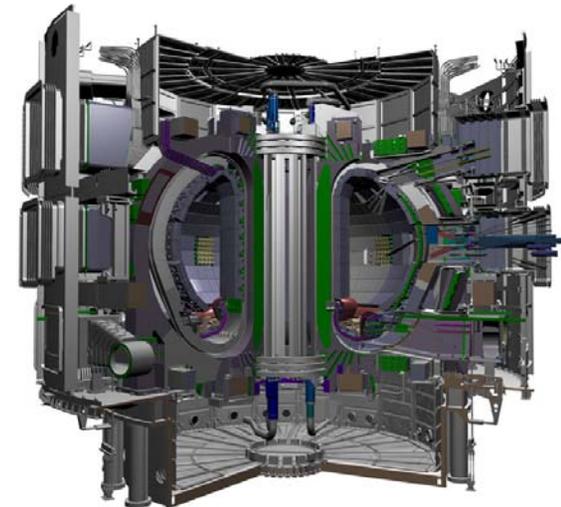


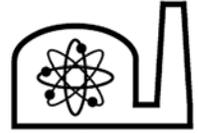
# Silicon Carbide Properties

- ❑ High strength at high temperature ( $>1000^{\circ}\text{C}$ ) and neutron fluence ( $>50$  DPA)
- ❑ Can withstand temperatures over  $2000^{\circ}\text{C}$
- ❑ Low chemical reactivity with fuel and water
- ❑ Smaller neutron absorption cross section than zircaloy
- ❑ In LWR core conditions
  - Little creep, high elastic modulus
  - Properties generally stable or quickly saturating with irradiation

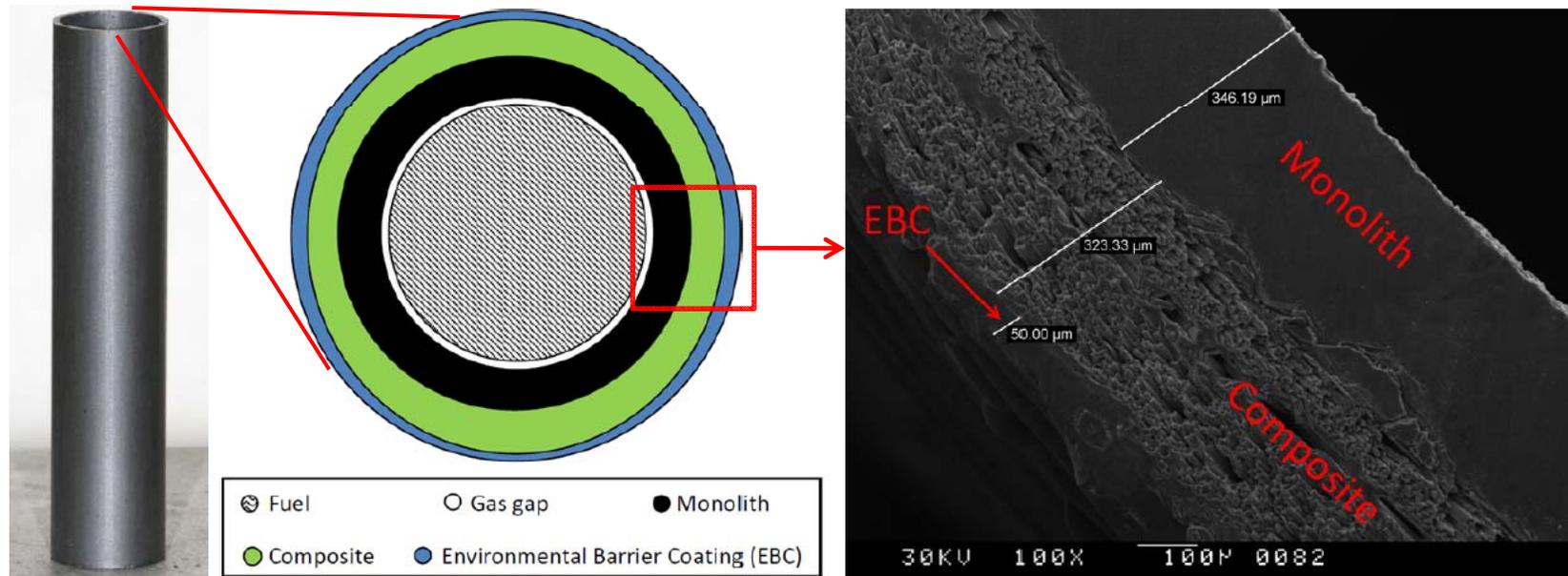


Saint-Gobain Ceramics

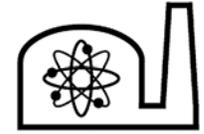




# SiC Triplex Cladding Design



- A multi-layered approach to maximize strength and minimize potential for cladding damage
  - Inner monolith for strength and hermetic gas seal (0.3 mm)
  - Woven fiber/matrix composite for strength and protection (0.3 mm)
  - Outer barrier coating to resist corrosion ( $\sim 100 \mu\text{m}$ )



# SiC Cladding Specimens



Zircaloy



Triplex



Triplex



Bond Test

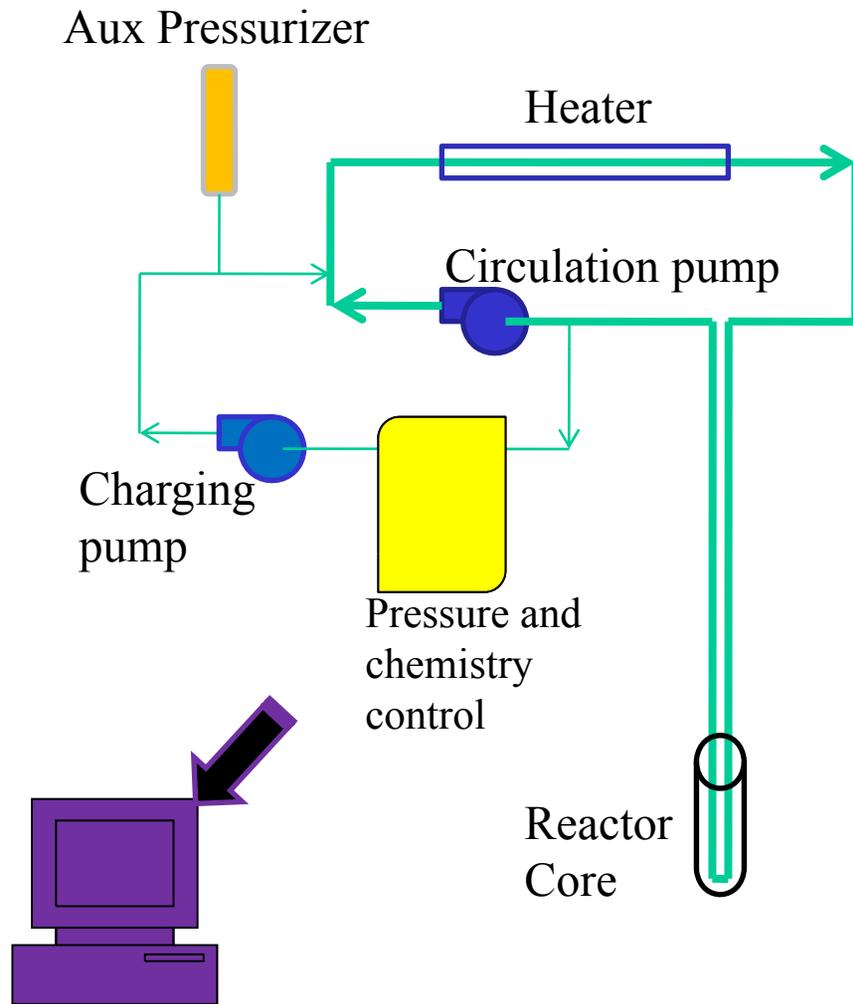


Irradiation  
Modules

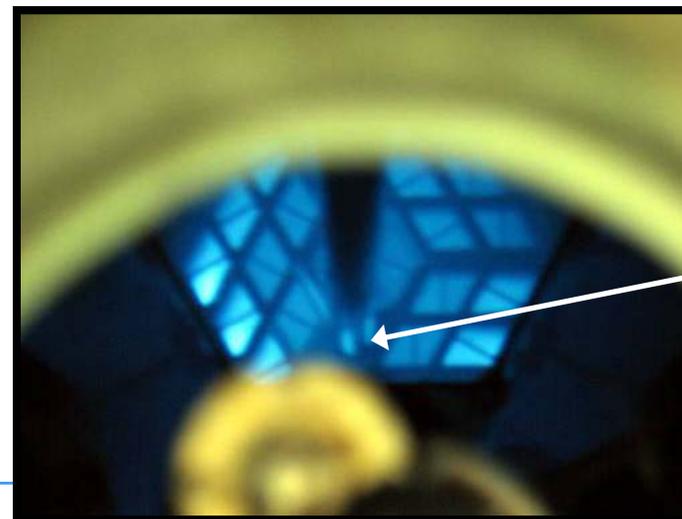




# Irradiation Loop Design



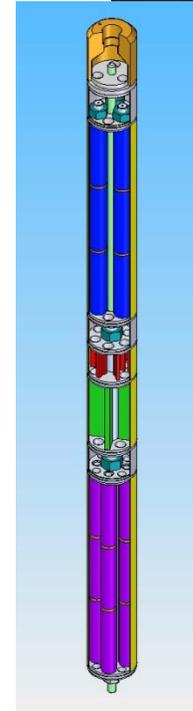
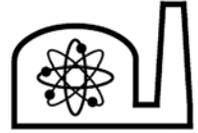
- Exposing prototype SiC cladding tubes to typical pressurized water reactor conditions
- Using a loop to achieve 300°C, 10 MPa, typical LWR flux, H<sub>2</sub> overpressure
- Max exposures >800 EFPD, >3000 MWd

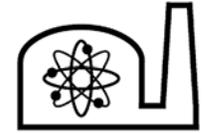


B-3 Irradiation Location

NRL

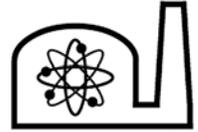
# Experiment Assembly





# Experiment Installation

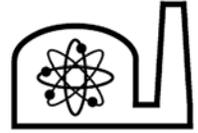




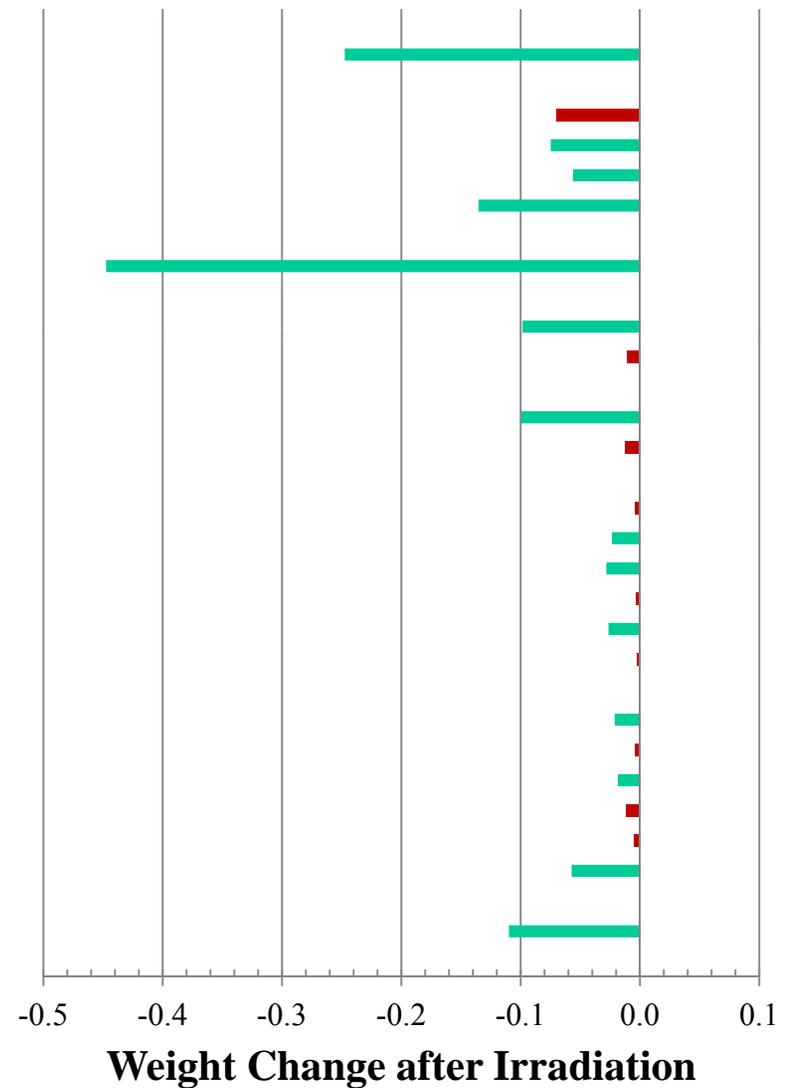
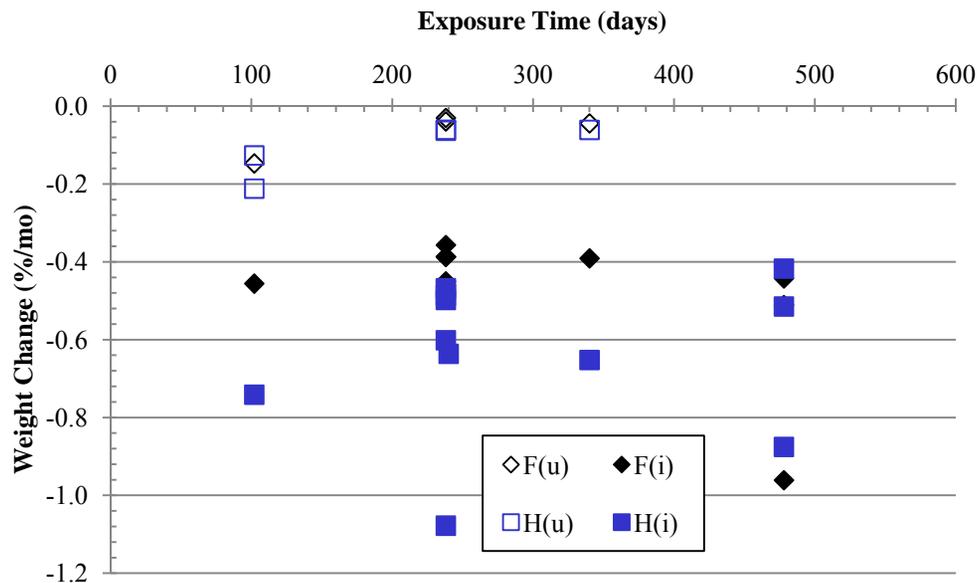
# Post-Irradiation Examinations

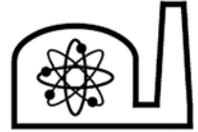
- ❑ Samples have been removed/replaced at intervals for weight change and dimensional measurements
  
- ❑ Destructive examinations
  - End-effect corrosion
  - Hoop strength
  - Thermal diffusivity
  - SEM

# Corrosion

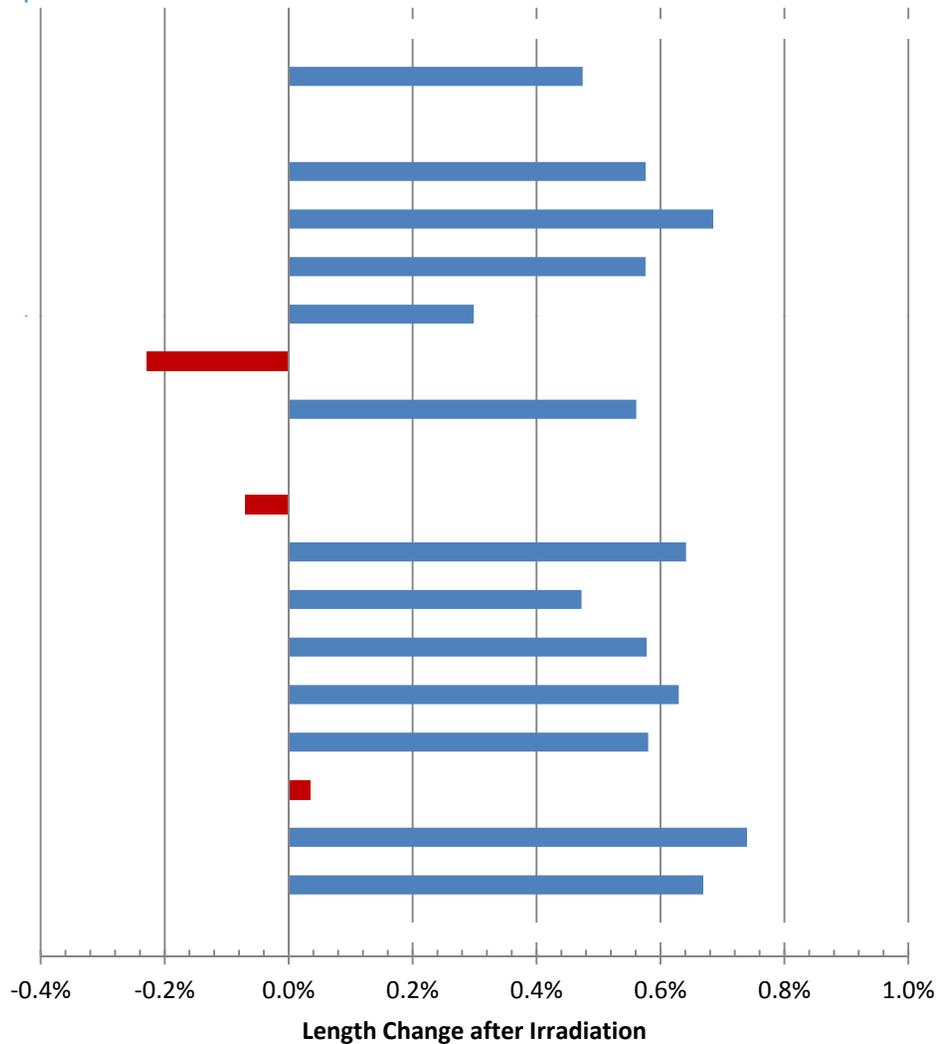


- Monolithic ( $\alpha$  and  $\beta$ ) SiC corrosion was negligible
- Composite is most vulnerable to corrosion, and CVI barrier coating provides best protection
- Weight change rates are constant over time
- Calculated surface recession based on weight loss
  - As low as  $0.5 \mu\text{m}/\text{mo}$  against  $100 \mu\text{m}$  thick EBC

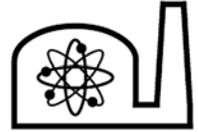




# Swelling



- Linear irradiation-induced swelling of CVD  $\beta$ -SiC will saturate  $\sim 0.6\%$ 
  - $\beta$ -SiC swelling is isotropic
  - Composite swelling is anisotropic
  - Swelling saturates within months



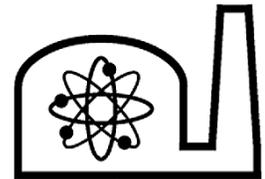
# Plug Testing

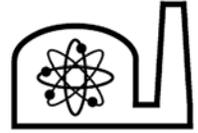
- A hydraulic ram compresses a urethane plug, and the plug expands inside of tube simulating internal pressurization





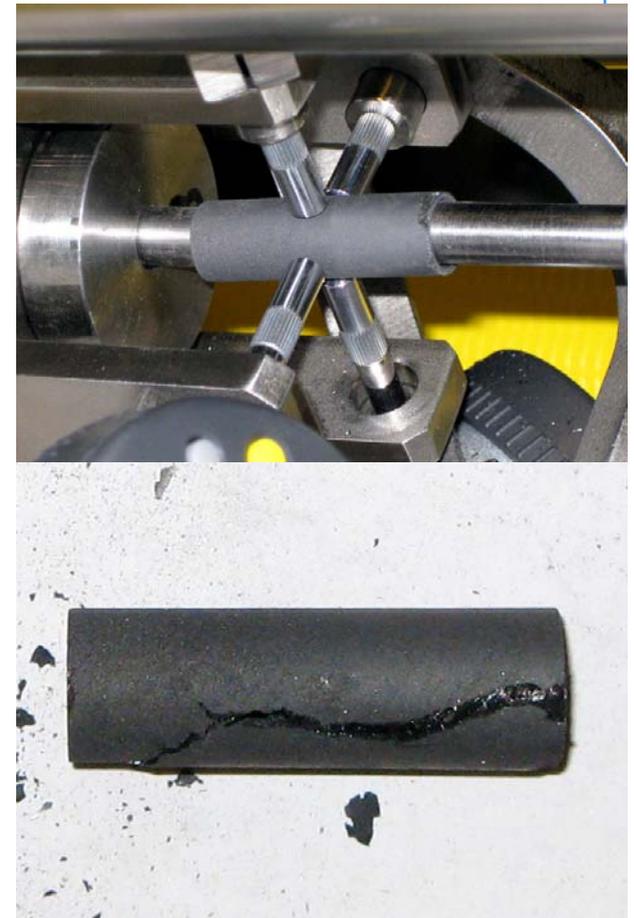
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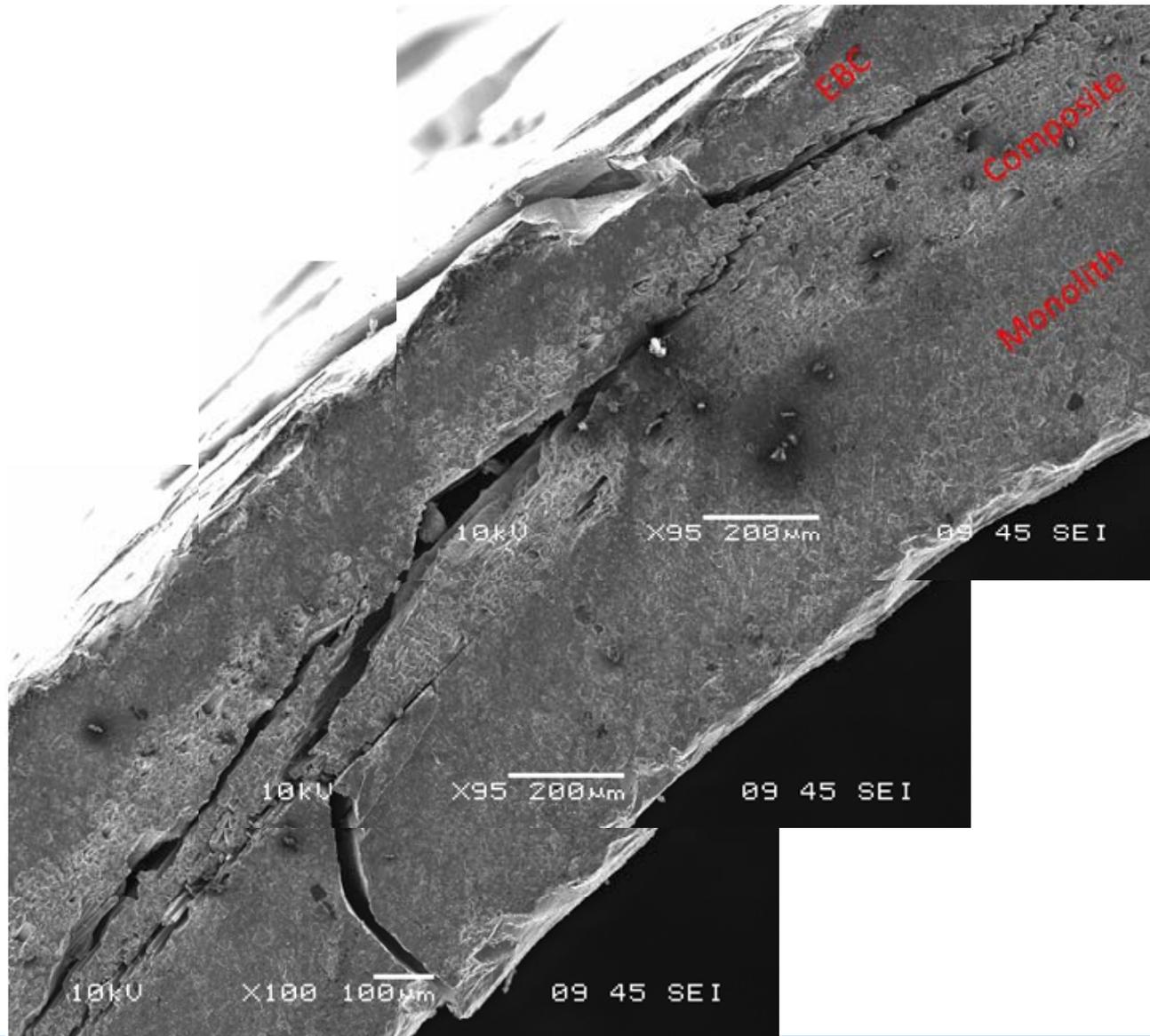
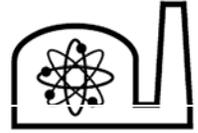


# Plug Testing

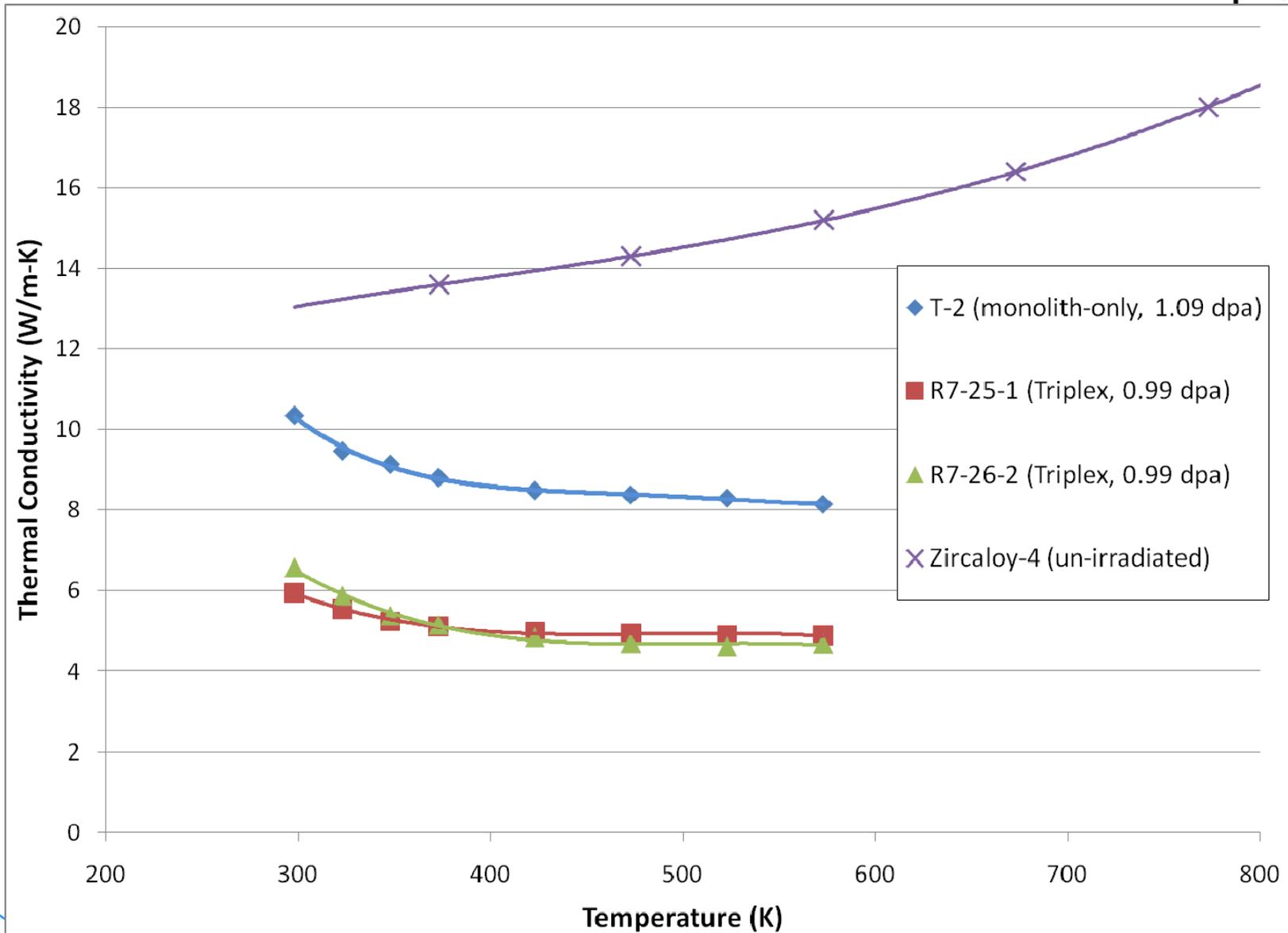
- ❑ All monolithic tubes failed with instant fragmentation
- ❑ Composite layer maintains integrity and internal fragments
- ❑ Triplex tubes are able to withstand additional strain after failure

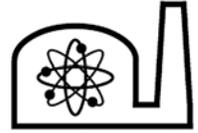


# Crack Propagation - SEM



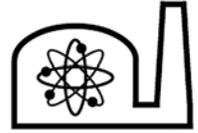
# Thermal Conductivity





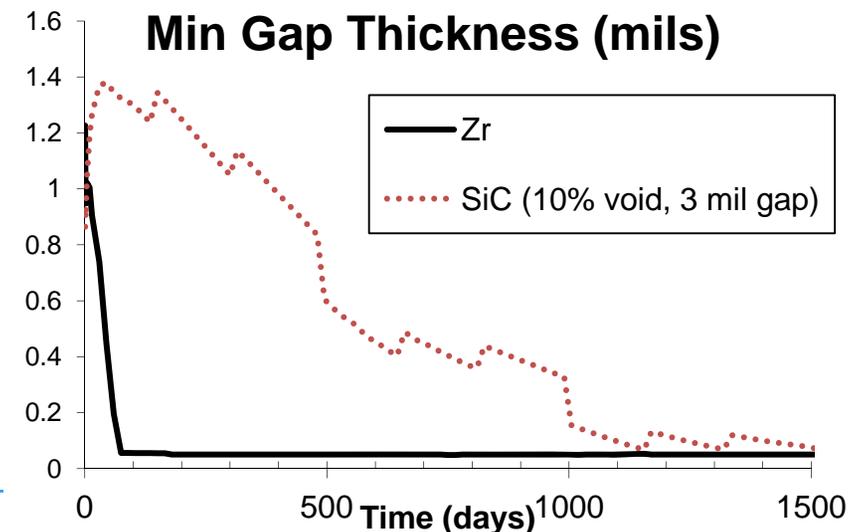
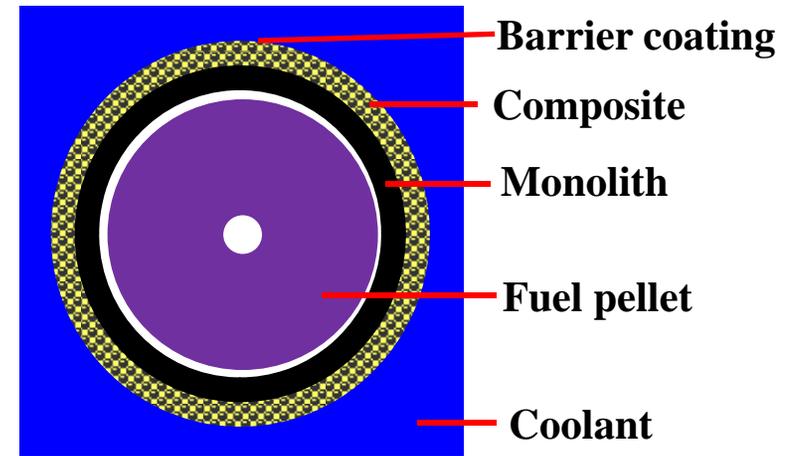
# Modeling In FRAPCON

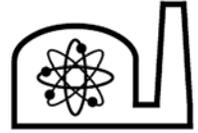
- ❑ FRAPCON evaluates a single fuel rod in steady-state LWR conditions
  - Code was developed to model  $\text{UO}_2$  and MOX fuel with zircaloy cladding to 65 MWd/kg in LWR conditions
  - High burnup fission gas release adjusted by Dr. Yun Long
  
- ❑ Previously implemented conservative SiC property models
  - Thermal conductivity, modulus, swelling, thermal expansion, creep
  
- ❑ Feedback from experimental work to FRAPCON
  - Swelling models are appropriate
  - Corrosion and crud deposition not a significant effect
  - Waiting on additional thermal diffusivity data
  - Tensile strength data used to check credibility of output



# FRAPCON Results

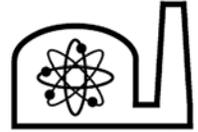
- ❑ Used SiC with annular pellet (10% central void)
  - Void reduces peak temperature at cost of fuel volume
  
- ❑ Good performance up to 100 MWd/kg (2500 days)
  - No FCMI until late in life
  - Fuel-cladding gap width drives fuel temperature
  
- ❑ Clad conductivity and open fuel-clad gap both contribute to elevated fuel temperatures
  - Improving gap conductance will alleviate other problems





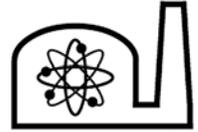
# Physics and Economics

- ❑ Reactivity and core reloading modeling
- ❑ Fuel cycle optimization and economics study
- ❑ Results
  - Physics of SiC clad cores similar to Zr clad
  - At comparable discharge burnup and fabrication costs, SiC has lower fuel cost
  - Larger SiC cost advantage at higher burnup – even larger advantage from 24 m cycles & uprate
- ❑ Fabrication cost adder for SiC is unlikely to eliminate SiC advantage



## Summary

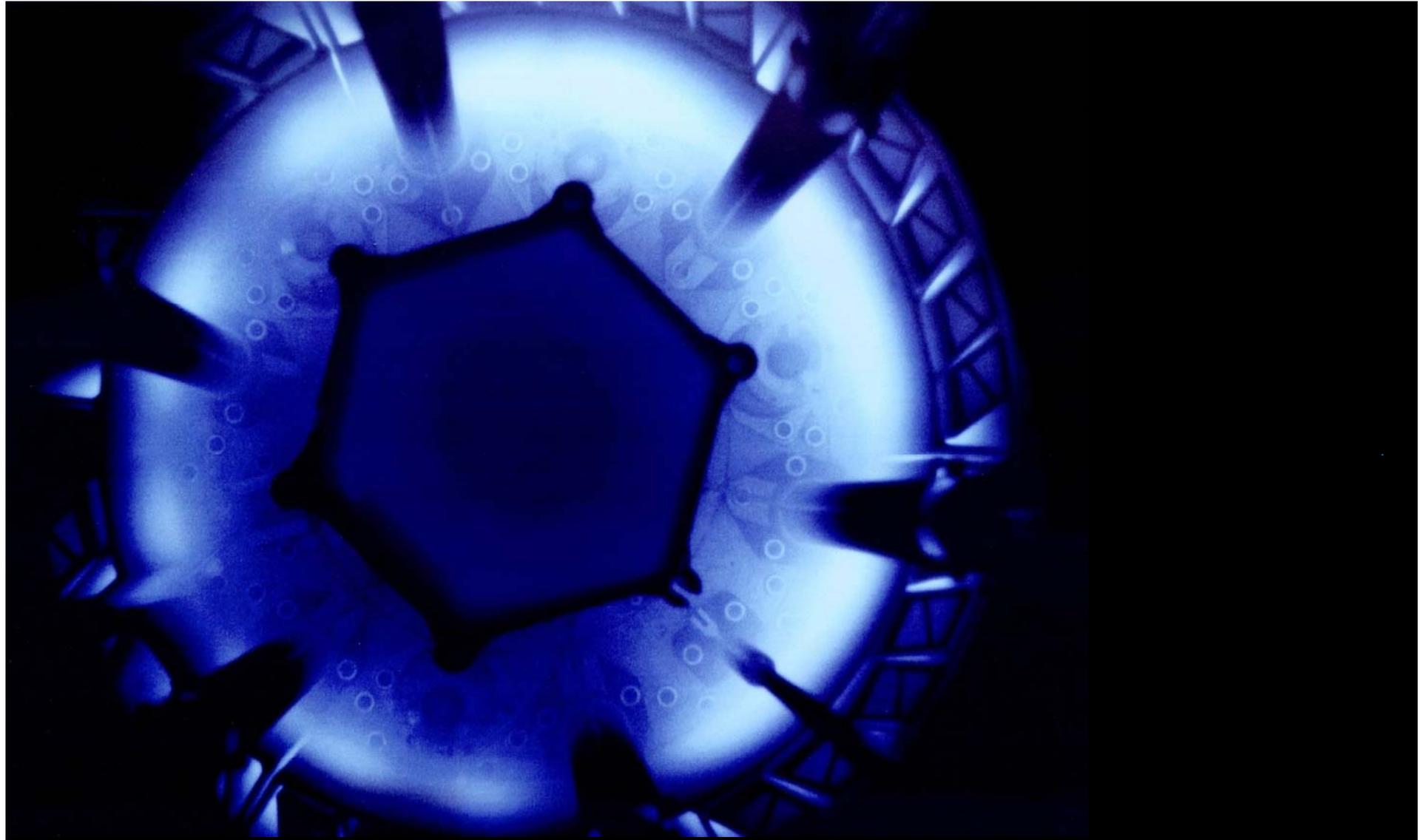
- ❑  $\beta$ -SiC is a promising material for LWR cladding, and the triplex cladding design combines the advantages of monolithic and fiber composite ceramics
- ❑ Irradiation experiments at the MIT reactor showed the corrosion, swelling, and strength behavior is acceptable in PWR conditions
- ❑ Computer modeling of the behavior of a SiC-clad fuel rod in typical PWR operating environment identified a need to adjust the fuel rod design to reduce fuel temperatures



# Thank You

## MIT Collaborators

- Prof. Mujid Kazimi
- Dr. Gordon Kohse
- Dr. Ed Pilat
- Dr. Sung Joong Kim
- Yakov Ostrovsky
- Jacob Dobisesky
- John Stempien
- Uuganbayar Otgonbaatar



Questions?